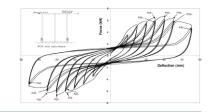


Date of issue: 21 February 2023



Steve Allison General Manager Premier Building Products Ltd

BTS2230-3 CERTIFICATE OF TEST: SUMMAY OF TESTS

Ten P21 Type Panel Bracing Capacity Tests of 10mm Standard PBP Gypsum Board

1. Objective:

- 1.1 BEAL Testing Services were contracted by Premier Building Products Ltd to assess the bracing capacity of the 10mm Standard PBP Gypsum Board.
- 1.2 Testing was carried out on single sets of specimens of the 10mm Standard Gypsum Board fixed to two sizes of timber framing that were prepared for testing by BEAL staff.

2. Methodology:

- 2.1 BEAL TP-211 ver1.0, is based on the test methodology titled **P21 A Wall bracing test and Evaluation Procedure**, published by BRANZ, updated in 2011.
- 2.2 The objective of this test procedure, is to evaluate the bracing capacity of walls and or wall panels, including Structural Insulated Panels (SIPs). After measurement and treatment of the data in accordance with the specified evaluation procedure, the wall or floor element can be assessed as contributing to the requirement of Clause B1.3.1 of the New Zealand Building Code.
- 2.3 A key requirement of this test procedure is an accurate description of all components used to construct the test specimen, including how the specimen is intended to be fixed or held down to the floor usually to a bottom plate.

3. Test Equipment:

3.1 To evaluate the bracing capacity of walls and or wall panels, a special mechanical test rig including a fast-acting hydraulic ram with calibrated load cell and displacement measuring device, with controls, is required.

4. Test Specimens:

4.1 Where BTS were not able to select the samples from a manufacturer or able to prepare the specimens, sampling shall follow the BEAL TP115 (BEAL Standard sampling procedure).

4.2 For this test, 10mm Gypsum Boards were supplied by the client, then fixed to two sizes of LVL timber framing, then installed into the BEAL mechanical test rig, by BEAL staff.

5. Specimen Conditioning – if any:

5.1 Specimens were installed at room conditions.

6. Test Criterion:

6.1 Unless specified by the client or selected by BEAL, the results obtained from this test procedure are to be assessed by a structural engineer with appropriate experience and skills.

7. Specimen Preparation:

- 7.1 The test methodology titled P21 A Wall bracing test and Evaluation Procedure, describes the requirements for the preparation and installation of the test panels into the mechanical test jig.
- 7.2 Generally, test specimens will be either 2,400mm, or 1,200mm, or 600mm or 400mm wide by 2,400mm in height. Timber frames of 1,200mm and 400mm wide were used.
- 7.3 For these tests, Premiere Building Products Gypsum board was tested one side. 400 mm panel length x 2400 mm panel height. 32mm x 6g GIB® Grabber® High Thread Screws at 50,100,150, 225, 300mm maximum from each corner and 150mm thereafter around the perimeter of the bracing element, 300mm maximum spacing to intermediate studs. No dwangs.
- 7.4 Pairs of hand driven 100 x 3.75mm nails at 600mm centres to baseplate with 20 mm particle board over 90x90 joist. Restrained block with three 100x4 mm nails to end studs the specified Gypsum Board was fixed to the timber frames on one side only.
- 7.5 To the end of the hydraulic ram, an attachment device is fixed onto the top plate of the test specimen. Refer photos.

8. Test Data:

The following information was provided by the client:

- a) Size of the panel:
- b) Overall thickness of the panel:
- c) description of each component:
- d) description of each type of fixing:
- e) description of any adhesives and or tapes used:
- f) description of fixing spacings:
- g) description of specified end of wall hold-down(s):
- h) Title of the technical and installation literature with version / date:

9. Analysis of the resulting test data:

- 9.1 An analysis of the force versus displacement data in csv format and converted into a scatter data graph with smooth lines, was made.
- 9.2 The resulting data file was forwarded to the structural engineer for further assessment.
- 9.3 The result of the engineers analysis is shown in Appendix A (at the back of this report).
- 9.4 The following were arrived at:

"All PBP bracing elements using the standard 10mm Gypsum Board with timber framing as per NZS3604 shall have fixing spacings at 50, 100, 150, 225, 300mm maximum from each corner and 150mm thereafter around the perimeter of the bracing element, with 300mm maximum spacing to intermediate stud or dwang.

Bracing elements with no HandiBrac® hold-down system, with bottom plate fixed as per NZS3604, can be used as a bracing element with the following bracing ratings:

Minimum length (m)	BU/m W	BU/m EQ
0.4	11.5	14.9
1.2	30.3	34.8

When the Gib HandiBrac® hold-down system is used in conjunction with 10mm PBP Standard Gypsum Board, it can be used as a bracing element with the following bracing ratings:

Minimum length (m)	BU/m W	BU/m EQ
1.2	75	64

10. Observations / Comment:

10.1 Graph TR221111-1 representing a 1,200mm wide x 2,400mm high specimen in KN vs mm, while Graph TR221111-2 representing a 400mm wide x 2,400mm high specimen in KN vs mm.

11. Attachments:

11.1 Report of representative graphs and resulting analysis.

- 11.2 Relevant Photos.
- 11.3 The csv and video files are available on request.

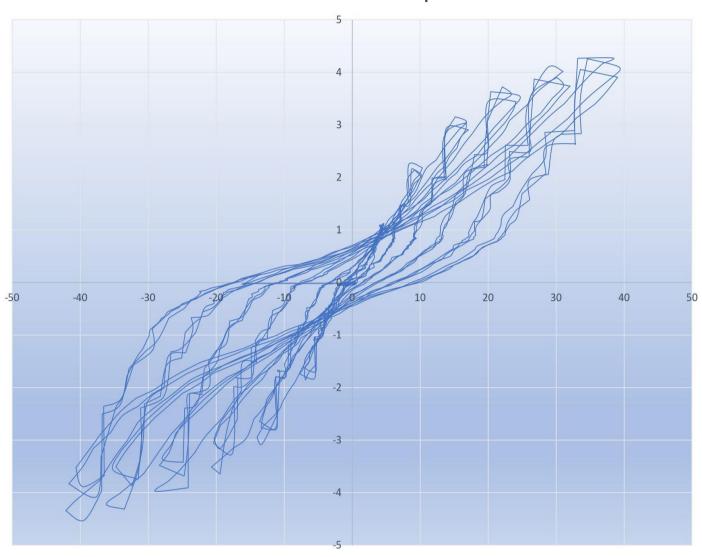
Colin Prouse – Senior Building Scientist

b. N. Maese.

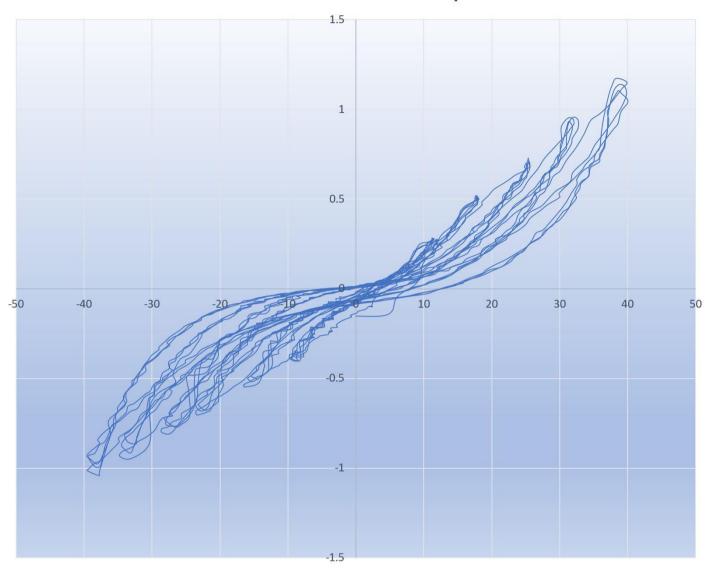
Building Element Assessment Laboratory Limited

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TR221111-1 P21 Force vs Displacement



TR221111-2 P21 Force versus Displacement





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12. APPENDIX A:

IOD: D==:=:	Duilding Droducts	LIOD NI=	10000	DECIONED	Page No.	TIA
IOB: Premiere	Building Products	JOB No.	10933	DESIGNER		TW
		DATE.		CHECKED		
21 Test Result A	nalvsis.			1200 mm	PBP Pane	els
				(with handi	-bracs)	
ample description:	Sample length	1.2	m	, with manual	2.465)	
32mm x 6g GIB® Gr. corner and 150mm spacing to intermed Pairs of hand driver over 90x90 joist. Ha	roducts Gypsum board of abber® High Thread Scre thereafter around the pe diate studs. No dwangs. In 100 x 3.75mm nails at 6 andi-brac brackets to stud th three 100x4 mm nails	ws at 50,100,1 erimeter of the 500mm centres d each end of p	50, 225, 30 bracing ele to basepla	0mm maxim ement, 300m te with 20 m	um from ea ım maximu m particle l	nch m board
value Nominate	e a target displacement (from the range	15 mm, 22	2 mm, 29 mn	n and 36 m	m)
	У	30	ļii i i i			
₈ values Loads ass	ociated with 8 mm displ	acement				
	Sample			_		
	TR230117-2	2.59	kN			
	TR230117-3	2.5	kN			
		2.0				
	TR230117-1	2.92	kN kN			
	TR230117-1	202 04 15	kN kN			
(1 value C - Avera	TR230117-1 ge residual displacement	2.92	kN	min 8mm dis	placement)
1 value C - Avera	ge residual displacement	2.92 t after first cycle	kN e (cycle to		placement)
1 value C - Avera		2.92	kN	min 8mm dis Average 3.12)
1 value C - Avera	ge residual displacement Sample	2.92 t after first cycle C+ (mm)	kN e (cycle to C- (mm)	Average	K1)
1 value C - Avera	ge residual displacement <u>Sample</u> TR230117-2	2.92 ct after first cycle C+ (mm) 2 1.93	kN e (cycle to C- (mm) -4.24 -3.12	Average 3.12	K1)
1 value C - Avera	ge residual displacement Sample TR230117-2 TR230117-3	2.92 t after first cycle C+ (mm) 2	kN e (cycle to C- (mm) -4.24	Average 3.12 2.53	K1 1.0 1.0)
' 1 value C - Avera _l	ge residual displacement Sample TR230117-2 TR230117-3	2.92 ct after first cycle C+ (mm) 2 1.93	c- (mm) -4.24 -3.12 -1.57	Average 3.12 2.53 2.30	K1 1.0 1.0 1.0	
	ge residual displacement Sample TR230117-2 TR230117-3 TR230117-1	2.92 C+ (mm) 2 1.93 3.03 $K1 = 1.4 - C$	kN e (cycle to C- (mm) -4.24 -3.12 -1.57 $C/8 \le 1.0$	Average 3.12 2.53 2.30 0.00 Note, reject	K1 1.0 1.0 1.0	
	ge residual displacement Sample TR230117-2 TR230117-3	2.92 C+ (mm) 2 1.93 3.03 $K1 = 1.4 - C$ Solute values of f	kN e (cycle to C- (mm) -4.24 -3.12 -1.57 $C/8 \le 1.0$ First cycle to	Average 3.12 2.53 2.30 0.00 Note, reject	K1 1.0 1.0 1.0	
(1 value C - Avera	ge residual displacement Sample TR230117-2 TR230117-3 TR230117-1 Py - Average of abso	$\begin{array}{c} 2.92 \\ \text{C+ (mm)} \\ \hline 2 \\ \hline 1.93 \\ \hline 3.03 \\ \hline K1 = 1.4 - C \\ \text{Olute values of f} \\ + \text{Py (kN)} \end{array}$	kN C- (mm) -4.24 -3.12 -1.57 $7/8 \le 1.0$ First cycle ko -Py (kN)	Average 3.12 2.53 2.30 0.00 Note, reject	K1 1.0 1.0 1.0	
	ge residual displacement Sample TR230117-2 TR230117-3 TR230117-1 Py - Average of abso	$\begin{array}{c} 2.92 \\ \text{C+ (mm)} \\ \hline 2 \\ \hline 1.93 \\ \hline 3.03 \\ \hline K1 = 1.4 - C \\ \text{Olute values of f} \\ + \text{Py (kN)} \\ \hline 5.17 \\ \end{array}$	kN e (cycle to C- (mm) -4.24 -3.12 -1.57 $C/8 \le 1.0$ First cycle (c) -Py (kN) -4.81	Average 3.12 2.53 2.30 0.00 Note, reject	K1 1.0 1.0 1.0	
	ge residual displacement Sample TR230117-2 TR230117-3 TR230117-1 Py - Average of abso TR230117-2 TR230117-3	$\begin{array}{c} 2.92 \\ \text{C+ (mm)} \\ \hline 2 \\ 1.93 \\ \hline 3.03 \\ K1 = 1.4 - C \\ \text{Olute values of f} \\ + \text{Py (kN)} \\ \hline 5.17 \\ \hline 5.03 \\ \end{array}$	kN e (cycle to C- (mm) -4.24 -3.12 -1.57 $C/8 \le 1.0$ First cycle to -Py (kN) -4.81 -4.18	Average 3.12 2.53 2.30 0.00 Note, reject pads 4.99 4.60	K1 1.0 1.0 1.0	
	ge residual displacement Sample TR230117-2 TR230117-3 TR230117-1 Py - Average of abso	$\begin{array}{c} 2.92 \\ \text{C+ (mm)} \\ \hline 2 \\ \hline 1.93 \\ \hline 3.03 \\ \hline K1 = 1.4 - C \\ \text{Olute values of f} \\ + \text{Py (kN)} \\ \hline 5.17 \\ \end{array}$	kN e (cycle to C- (mm) -4.24 -3.12 -1.57 $C/8 \le 1.0$ First cycle (c) -Py (kN) -4.81	Average 3.12 2.53 2.30 0.00 Note, reject	K1 1.0 1.0 1.0	
	ge residual displacement Sample TR230117-2 TR230117-3 TR230117-1 Py - Average of abso TR230117-2 TR230117-3	$\begin{array}{c} 2.92 \\ \text{C+ (mm)} \\ \hline 2 \\ 1.93 \\ \hline 3.03 \\ K1 = 1.4 - C \\ \text{Olute values of f} \\ + \text{Py (kN)} \\ \hline 5.17 \\ \hline 5.03 \\ \end{array}$	kN e (cycle to C- (mm) -4.24 -3.12 -1.57 $C/8 \le 1.0$ First cycle to -Py (kN) -4.81 -4.18	Average 3.12 2.53 2.30 0.00 Note, reject pads 4.99 4.60	K1 1.0 1.0 1.0	
	ge residual displacement Sample TR230117-2 TR230117-3 TR230117-1 Py - Average of abso TR230117-2 TR230117-3	$\begin{array}{c} 2.92 \\ \text{C+ (mm)} \\ \hline 2 \\ 1.93 \\ \hline 3.03 \\ K1 = 1.4 - C \\ \text{Olute values of f} \\ + \text{Py (kN)} \\ \hline 5.17 \\ \hline 5.03 \\ \end{array}$	kN e (cycle to C- (mm) -4.24 -3.12 -1.57 $C/8 \le 1.0$ First cycle to -Py (kN) -4.81 -4.18	Average 3.12 2.53 2.30 0.00 Note, reject pads 4.99 4.60	K1 1.0 1.0 1.0	
	ge residual displacement Sample TR230117-2 TR230117-1 Py - Average of abso TR230117-2 TR230117-3 TR230117-1	2.92 C+ (mm) 2 1.93 3.03 $K1 = 1.4 - C$ Polyte values of f +Py (kN) 5.17 5.03 5.44	C- (mm) -4.24 -3.12 -1.57 C/8 ≤ 1.0 First cycle to -Py (kN) -4.81 -4.18 -4.77	Average 3.12 2.53 2.30 0.00 Note, reject bads 4.99 4.60 5.11	K1 1.0 1.0 1.0	
	ge residual displacement Sample TR230117-2 TR230117-3 TR230117-1 Py - Average of abso TR230117-2 TR230117-3	$\begin{array}{c} 2.92 \\ \text{C+ (mm)} \\ \hline 2 \\ 1.93 \\ \hline 3.03 \\ K1 = 1.4 - 6 \\ \text{olute values of f} \\ + \text{Py (kN)} \\ \hline 5.17 \\ \hline 5.03 \\ \hline 5.44 \\ \text{olute values of f} \\ \end{array}$	c (cycle to C- (mm) -4.24 -3.12 -1.57 C/8 ≤ 1.0 First cycle lo -Py (kN) -4.81 -4.18 -4.77	Average 3.12 2.53 2.30 0.00 Note, reject bads 4.99 4.60 5.11	K1 1.0 1.0 1.0	
	Sample TR230117-2 TR230117-3 TR230117-1 Py - Average of abso TR230117-2 TR230117-3 TR230117-1 Ry - Average of abso	2.92 C+ (mm) 2 1.93 3.03 K1 = 1.4 - C Olute values of f +Py (kN) 5.17 5.03 5.44 Olute values of f +Ry (kN)	c (cycle to C- (mm) -4.24 -3.12 -1.57 C/8 ≤ 1.0 First cycle lo -Py (kN) -4.81 -4.18 -4.77 Py Fourth cycle -Ry (kN)	Average 3.12 2.53 2.30 0.00 Note, reject bads 4.99 4.60 5.11 4.90	K1 1.0 1.0 1.0	
	Sample TR230117-2 TR230117-3 TR230117-1 Py - Average of abso TR230117-2 TR230117-3 TR230117-1 Ry - Average of abso	2.92 C+ (mm) 2 1.93 3.03 K1 = 1.4 - C Olute values of f +Py (kN) 5.17 5.03 5.44 Olute values of f +Ry (kN) 4.24	c (cycle to C- (mm) -4.24 -3.12 -1.57 C/8 ≤ 1.0 First cycle lo -Py (kN) -4.81 -4.18 -4.77 Py Fourth cycle -Ry (kN) -3.52	Average 3.12 2.53 2.30 0.00 Note, reject pads 4.99 4.60 5.11 4.90	K1 1.0 1.0 1.0	
	Sample TR230117-2 TR230117-3 TR230117-1 Py - Average of abso TR230117-2 TR230117-3 TR230117-1 Ry - Average of abso	2.92 C+ (mm) 2 1.93 3.03 K1 = 1.4 - C Olute values of f +Py (kN) 5.17 5.03 5.44 Olute values of f +Ry (kN) 4.24 4.25	C- (mm) -4.24 -3.12 -1.57 C/8 ≤ 1.0 First cycle ld -Py (kN) -4.81 -4.18 -4.77 Py Fourth cycle -Ry (kN) -3.52 -3.34	Average 3.12 2.53 2.30 0.00 Note, reject ads 4.99 4.60 5.11 4.90 es 3.87 3.67	K1 1.0 1.0 1.0	
	Sample TR230117-2 TR230117-3 TR230117-1 Py - Average of abso TR230117-2 TR230117-3 TR230117-1 Ry - Average of abso	2.92 C+ (mm) 2 1.93 3.03 K1 = 1.4 - C Olute values of f +Py (kN) 5.17 5.03 5.44 Olute values of f +Ry (kN) 4.24	c (cycle to C- (mm) -4.24 -3.12 -1.57 C/8 ≤ 1.0 First cycle lo -Py (kN) -4.81 -4.18 -4.77 Py Fourth cycle -Ry (kN) -3.52	Average 3.12 2.53 2.30 0.00 Note, reject pads 4.99 4.60 5.11 4.90	K1 1.0 1.0 1.0	
	Sample TR230117-2 TR230117-3 TR230117-1 Py - Average of abso TR230117-2 TR230117-3 TR230117-1 Ry - Average of abso	2.92 C+ (mm) 2 1.93 3.03 K1 = 1.4 - C Olute values of f +Py (kN) 5.17 5.03 5.44 Olute values of f +Ry (kN) 4.24 4.25	C- (mm) -4.24 -3.12 -1.57 C/8 ≤ 1.0 First cycle ld -Py (kN) -4.81 -4.18 -4.77 Py Fourth cycle -Ry (kN) -3.52 -3.34	Average 3.12 2.53 2.30 0.00 Note, reject ads 4.99 4.60 5.11 4.90 es 3.87 3.67	K1 1.0 1.0 1.0	
	Sample TR230117-2 TR230117-3 TR230117-1 Py - Average of abso TR230117-2 TR230117-3 TR230117-1 Ry - Average of abso	2.92 C+ (mm) 2 1.93 3.03 K1 = 1.4 - C Olute values of f +Py (kN) 5.17 5.03 5.44 Olute values of f +Ry (kN) 4.24 4.25	C- (mm) -4.24 -3.12 -1.57 C/8 ≤ 1.0 First cycle ld -Py (kN) -4.81 -4.18 -4.77 Py Fourth cycle -Ry (kN) -3.52 -3.34	Average 3.12 2.53 2.30 0.00 Note, reject ads 4.99 4.60 5.11 4.90 es 3.87 3.67	K1 1.0 1.0 1.0	

